

A rigorous method to calculate the rising speed of gas kick

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Abstract The rising speed of gas kick is an important parameter in well control operation. The position of the gas kick dictates the pressure at the casing shoe, which is usually the weakest point in the openhole section, and the wellhead pressure, which is one of the key factors affecting the blowout preventer and choke folder. In this research, we derived a rigorous model to estimate the rising speed of gas kick. Starting from the force analysis and mass conservation, we developed equations to calculate the forces exerting on the gas kick. With the mass of the gas kick, the rising speed of the gas kick is calculated. The effect of wellbore temperature profile on the rising of the gas kick is taken into account in the derivation. Before the development of this model, the estimation of gas kick position is commonly based on experience. In many cases, the experience alone is not good enough for well control. The proposed model provides a new approach with solid theoretical base to characterize the rising of gas kick in the hole. It makes the procedure of the well control simple and makes drilling engineers feel more comfortable to control the well. The new model can be combined with engineers experience to predict the downhole situation, shut-in casing pressure, and mud rate as a functions of position of gas kick. Any deviation from the forecast indicates accidents or downhole problems. Therefore, the proposed model is a valuable tool to diagnose the problems in well control.

Keywords Gas kick · Well control · Kick migration speed

Nomenclature

$A_{\text{cone base}}$	= Area of base of cone of gas column
$A_{\text{cone surface}}$	= Characteristic area of the cone of gas column
$A_{\text{gas column base}}$	= Area of base of gas column
$A_{\text{gas column flank}}$	= Surface area of flank of gas column
a	= Acceleration
D_1	= Drillpipe diameter
D_2	= Wellbore diameter
E_k	= Kinetic energy per unit volume
F_1	= Fluid force behind the gas column
F_2	= Fluid force in front of the gas column
F_{D1}	= Drag force on the flank of the gas column
F_{D2}	= Drag force on the cone surface of gas column
$F_{D2\text{-}Vert}$	= Vertical drag force resulting from drag force on the cone surface of gas column
F_G	= Gravitational force
F_{net}	= Net force
f	= Friction factor
f_i	= Gas-mud interfacial friction factor
g	= Gravitational acceleration
$h_{\text{gas base}}$	= Location of base of gas column
$h_{\text{gas center}}$	= Location of center of gas column
h_{well}	= Well depth
K	= Consistency index of mud
$L_{\text{bottomhole-gas base}}$	= Distance between bottomhole and base of gas column
$L_{\text{gas cone}}$	= Height of cone part of gas kick

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$L_{\text{gas cylinder}}$	= Height of cylinder part of gas kick
$L_{\text{gas kick}}$	= Height of gas kick
L_{migrated}	= Gas migrated distance
$L_{\text{wellhead-gas top}}$	= Distance between wellhead and top of gas column
M	= Molecular weight of gas
m_g	= Mass of gas column
n	= Flow-behavior index of mud
p_1	= Pressure behind the gas column
p_2	= Pressure in front of the gas column
p_{casing}	= Casing pressure
p_f	= Frictional pressure drop
p_p	= Pore pressure
p_{SIDP}	= Shut-in drillpipe pressure
\bar{p}_{gas}	= Average pressure of gas column
R	= Universal gas constant
T	= Temperature at location
T_{BH}	= Bottomhole temperature
u_g	= Gas velocity
u_m	= Mud velocity
$V_{\text{gas cone}}$	= Volume of cone part of gas kick
$V_{\text{gas cylinder}}$	= Volume of cylinder part of gas kick
$V_{\text{gas kick}}$	= volume of gas kick at any location
$V_{\text{gas kick,BH}}$	= Volume of gas kick at bottomhole
$V_{M,\text{out}}$	= Volume of mud flow out the hole
$V_{M,\text{in}}$	= Volume of mud flow into the hole
z	= gas deviation factor
z_{BH}	= Gas deviation factor at bottomhole
ρ_g	= Gas density
$\rho_{g,\text{BH}}$	= Gas density at bottomhole
ρ_m	= Mud density
θ	= Angle between F_{D2} and vertical direction
θ_{300}	= The 300-rpm dial reading in mud viscometer
θ_{600}	= The 600-rpm dial reading in mud viscometer
μ_g	= Gas viscosity
τ_{gm}	= Shear stress between gas and mud
Δt_I	= 1st time step

Introduction

The rising speed of gas kick is an important parameter in well control operation. The position of the gas kick dictates the pressure at the casing shoe, which is usually the weakest point in the openhole section, and the wellhead pressure, which is one of the key factors affecting the blowout preventer and choke folder. In many gas kick well control operations, the estimations of gas kick position are commonly based on experience. In many cases, the

experience alone is not good enough for well control. A model with theoretical base to predict the gas kick rising speed is highly desired.

Many studies have been focused on gas–liquid two-phase flow in wellbore. Some researchers developed model to analyze two-phase flow in annuli during drilling. LeBlanc and Lewis (1968) built a mathematical model to calculate the backpressure during circulating gas kick out of well. In their model, the frictional pressure drop was ignored. Hoberock and Stanbery (1981a, b) combined different models to analyzed pressure distribution in wells during gas kicks assuming constant temperature along the annulus. Santos and Bourgoyne (1989) estimated pressure profile in wellbore for two-phase flow basing on flow regime. Van Slyke and Huang (1990) used a dynamic wellbore model to predict gas kick behavior in oil-based drilling mud. The mass of free gas changes with the temperature and pressure because the solution gas in oil-base mud varies along the wellbore. Johnson and White (1991) conducted experiment to examine gas migration rate in drilling mud in a 49-ft long, 7.8-in ID inclinable flow loop. Skalle et al. (1991) studied gas rising velocity and its effect on bottomhole pressure (BHP) in a vertical well using experiment. Three empirical two-phase flow correlations were used to analyze the experimental data. Frank and Rolv (1991) ran full-scale kick experiments and studied the effect of different parameters on gas-rise velocity. Johnson and Steven (1993) investigated the gas migration velocities during gas kicks in deviated wells using the same facilities used by Johnson and White in 1991. Martins Lage et al. (1994) tested the gas kick migration in closed and open wells. Tarvin et al. (1994) analyzed data from test-well experiment and found that gas rises through drilling mud faster than the migration rates generally accepted in the drilling industry. Ashley et al. (1995) reviewed different gas migration velocity at different gas concentration. Choe (2001) developed a two-phase flow model to calculate pressure in annulus using flow regime. Nunes et al. (2002) used Beggs and Brill method to analyze gas kicks in deepwater well drilling. Yu et al. (2009) developed a mechanistic model for gas–liquid flow in upward vertical annuli. Flow regimes are applied in their model. Chirinos et al. (2011) proposed a simplified method to estimate peak casing pressure during managed pressure drilling well control.

Methods to detect a kick

It is crucial to detect a kick as the early beginning. Early detection can minimize the kick size and reduce the risk of blowout when controlling the well. Kick-detection equipment should be installed. The followings are important kick indications:

1. An abrupt increase in penetration rate or drilling break
2. An increase in pump rate and a decrease in pump pressure
3. An increase in the mud return flow rate
4. Pit gains due to the increase in the mud return flow rate
5. An increase in drillstring weight
6. Gas cutting or salinity changes in the drilling fluid
7. Mud flows when pumps are off.
5. Circulate kill mud until it flows out of the choke
6. Reduce pump speed while closing the choke
7. Shut down the pump
8. Check casing pressure and drillpipe pressure to make sure both pressures are zero psi
9. If both pressures are zero psi, complete well control.

Well control procedures to circulate out gas kick and kill the well

When there is a kick, two methods are usually applied to circulate the kick out of the wellbore and keep the well under control. They are driller's method and wait and weight method. A thoroughly understanding of procedures of these two well control methods helps the development of governing equation for gas kick rising speed calculation. The basic principle of both methods is to keep BHP constant at the formation pressure. The driller's method differs from wait and weight method in the circulation number. Driller's method needs two circulations to circulate the kick out of hole and kill the well. Following steps are used in driller's method:

1. Shut in the well and get casing pressure and drillpipe pressure
2. Calculate the kill mud weight
3. Start up the pump by holding casing pressure constant
4. Pump old mud and circulate the kick out of hole while keeping drillpipe pressure constant
5. After circulating kick out of hole, pump kill mud; start up the pump by holding casing pressure constant
6. Hold casing pressure constant and pump kill mud until kill mud flow to the bit
7. Switch to constant drillpipe pressure and circulate kill mud until it flows out of the choke
8. Shut down pumps by holding casing pressure constant
9. Check casing pressure and drillpipe pressure to make sure both pressures are zero psi
10. If both pressures are zero psi, complete well control.

The procedure of wait and weight method is as follows:

1. Shut in the well and get casing pressure and drillpipe pressure
2. Calculate the kill mud weight and mix the kill mud
3. Start up the pump by holding casing pressure constant
4. Pump kill mud and circulate the kick out of hole while keeping BHP constant, manipulate the choke to make sure drillpipe pressure, and follow the pressure reduction schedule

Gas kick rising speed in well control

According to the procedure of driller's method, the old mud is pumped into the drillpipe to circulate the kick out of the hole, which occurs in the first circulation. Therefore, the mud in drillpipe and annulus has same properties. To analyze the gas kick rising speed during the circulation, following assumptions are made:

1. A volume of gas kick, $V_{g,BH}$, entered into the bottomhole when the well is shut in
2. The compressibility of mud is neglected comparing with gas compressibility
3. Gas kick rises from the bottomhole to surface as a single column
4. There are two mud annuli between gas column and walls of wellbore and drillpipe due to the wettability effect. The thicknesses of these two annuli are very small comparing with the radius of the gas column
5. The temperature of gas column follows the temperature gradient in mud
6. Water base mud with negligible gas solubility
7. Drilling mud follows power-law model.

For a volume of gas kick, $V_{g,BH}$, enters into the bottomhole, the volume of the gas kick equals the difference between the mud flow out of hole and into the hole.

$$V_{\text{gas kick,BH}} = V_{M,\text{out}} - V_{M,\text{in}} \quad (1)$$

where $V_{\text{gas kick,BH}}$ = volume of gas kick at bottomhole, $V_{M,\text{out}}$ = volume of mud flow out the hole, $V_{M,\text{in}}$ = volume of mud flow into the hole.

Since the time period between well shut in and starting pumping old mud to circulate the kick is very short, we can assume the migration of gas begin as the pump is started up. Now we analyze the rising speed of gas column at the beginning of first circulation. As old mud is pumped into the drillpipe, the gas kick migrates upward inside the annulus like a piston as shown in Fig. 1. At the time the gas kick begins to move upward, the height of gas kick is the sum of heights of cone part and cylinder part, which is expressed as

$$L_{\text{gas kick}} = L_{\text{gas cone}} + L_{\text{gas cylinder}} \quad (2)$$

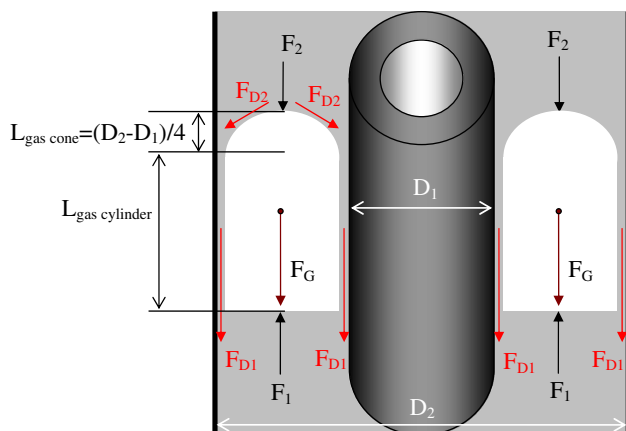


Fig. 1 Distribution of gas kick in the annuli

where $L_{\text{gas kick}}$ = height of gas kick, $L_{\text{gas cone}}$ = height of cone part of gas kick, $L_{\text{gas cylinder}}$ = height of cylinder part of gas kick.

Due to the effect of gas–mud interfacial tension, the height of cone should equal $\frac{D_2 - D_1}{4}$ assuming the annuli between gas column and walls of wellbore and drillpipe are small and can be neglected. Therefore, the volume of gas kick can be expressed as

$$\begin{aligned}
 V_{\text{gas kick}} &= V_{\text{gas cone}} + V_{\text{gas cylinder}} \\
 &= 2\pi \left(\frac{D_1}{2} + \frac{D_2 - D_1}{4} \right) \frac{\pi (D_2 - D_1)^2}{16} \\
 &\quad + \pi \frac{D_2^2 - D_1^2}{4} L_{\text{gas cylinder}} \\
 &= \pi^2 \left(\frac{D_2^2 - D_1^2}{4} \right) \left(\frac{D_2 + D_1}{16} \right) + \pi \frac{D_2^2 - D_1^2}{4} L_{\text{gas cylinder}}
 \end{aligned} \quad (3)$$

where $V_{\text{gas kick}}$ = volume of gas kick at any location, $V_{\text{gas cone}}$ = volume of cone part of gas kick, $V_{\text{gas cylinder}}$ = volume of cylinder part of gas kick, D_1 = drillpipe diameter, D_2 = wellbore diameter.

Therefore, the height of gas cylinder can be estimated from gas kick volume, which is

$$\begin{aligned}
 L_{\text{gas cylinder}} &= \frac{V_{\text{gas kick}} - \pi^2 \left(\frac{D_2^2 - D_1^2}{4} \right) \left(\frac{D_2 + D_1}{16} \right)}{\pi \frac{D_2^2 - D_1^2}{4}} \\
 &= \frac{V_{\text{gas kick}}}{\pi \frac{D_2^2 - D_1^2}{4}} - \pi \left(\frac{D_2 + D_1}{16} \right)
 \end{aligned} \quad (4)$$

As the gas column moves upward, the gas expands. According to Eq. (4), the shape of gas cone remains constant while the height of gas cylinder becomes longer due to gas expansion.

To estimate the rising velocity of gas kick, force analysis is required. Forces on gas column can be analyzed in

two dimensions, horizontal and vertical directions. For the purpose of this study, horizontal forces are not considered. According to the U-tube theory, the pressure inside the drillpipe should be balanced by pressure in the annulus. When the old mud is pumped into the drillpipe, the gas column will move upward along the annulus. The gas column is subjected to five forces, the gravitational force, the drag force on the cone surface of gas column, the drag force on the flank of the gas column, the fluid forces in front of and behind the gas column. Because the forces in the vertical direction control the upward movement of gas kick, they are analyzed here. The net force in vertical direction is calculated by

$$F_{\text{net}} = F_1 - F_2 - F_{D1} - F_{D2-\text{Vert}} - F_G$$

or

$$F_{\text{net}} = F_1 - F_2 - F_{D1} - \int_0^{90^\circ} F_{D2} \cos \theta d\theta - F_G \quad (5)$$

where F_{net} = net force, F_G = gravitational force, F_{D2} = drag force on the cone surface of gas column, $F_{D2-\text{Vert}}$ = vertical drag force resulting from drag force on the cone surface of gas column, F_{D1} = drag force on the flank of the gas column, F_2 = fluid force in front of the gas column, F_1 = fluid force behind the gas column, θ = angle between F_{D2} and vertical direction.

The fluid force behind the gas column is

$$F_1 = p_1 A_{\text{gas column base}} = \pi \frac{D_2^2 - D_1^2}{4} p_1 \quad (6)$$

where p_1 = pressure below the gas column, $A_{\text{gas column base}}$ = area of base of gas column.

According to the basic principle in the driller's and engineer's methods, BHP is kept constant during the circulation, which means BHP always equals pore pressure. Therefore, the pressure below the gas column can be expressed in terms of pore pressure, frictional pressure drop, and pressure change due to potential energy change, which is

$$p_1 = p_p - \rho_m g L_{\text{bottomhole-gas base}} - p_f \quad (7)$$

where p_p = pore pressure, ρ_m = mud density, g = gravitational acceleration, $L_{\text{bottomhole-gas base}}$ = distance between bottomhole and base of gas column, p_f = frictional pressure drop between bottomhole and base of gas column.

Pore pressure can be estimated from the shut-in drillpipe pressure and static hydraulic pressure due to drill mud, which is

$$p_p = p_{\text{SIDP}} + \rho_m g h_{\text{well}} \quad (8)$$

where p_{SIDP} = shut-in drillpipe pressure, h_{well} = well depth.

The frictional pressure drop depends on the flow regime. When the Reynolds number is less than 2,100, the flow is laminar; otherwise, it is turbulent flow. The Reynolds number is calculated through (Bourgoyne et al. 1986)

$$N_{Re} = \frac{109000 \rho_m u_m^{2-n}}{K} \left[\frac{0.0208 (D_2 - D_1)}{2 + 1/n} \right]^n \quad (9)$$

where

$$K = \frac{510 \theta_{300}}{511^n} \quad (10)$$

$$n = 3.32 \log \frac{\theta_{600}}{\theta_{300}} \quad (11)$$

where K = consistency index of mud, n = flow-behavior index of mud, u_m = mud velocity, θ_{300} = the 300-rpm dial reading in mud viscometer, θ_{600} = the 600-rpm dial reading in mud viscometer.

If the flow is laminar flow, the frictional pressure drop can be calculated by (Bourgoyne et al. 1986)

$$p_f = \frac{dp_f}{dh} L_{\text{bottomhole-gas base}} = \frac{K u_m^n \left(\frac{2+1/n}{0.0208} \right)^n}{144000 (D_2 - D_1)^{1+n}} L_{\text{bottomhole-gas base}} \quad (12)$$

If the flow is turbulent flow, the frictional pressure drop can be calculated by

$$p_f = \frac{dp_f}{dh} L_{\text{bottomhole-gas base}} = \frac{f \rho_m u_m^2}{21.1 (D_2 - D_1)} L_{\text{bottomhole-gas base}} \quad (13)$$

where f = friction factor.

The friction factor can be read from Fig. 2.

The fluid force in front of the gas column is

$$F_2 = p_2 A_{\text{cone base}} = p_2 A_{\text{gas column base}} = \pi \frac{D_2^2 - D_1^2}{4} p_2 \quad (14)$$

where p_2 = pressure in front of the gas column, $A_{\text{cone base}}$ = area of base of cone of gas column, which equals area of base of gas column.

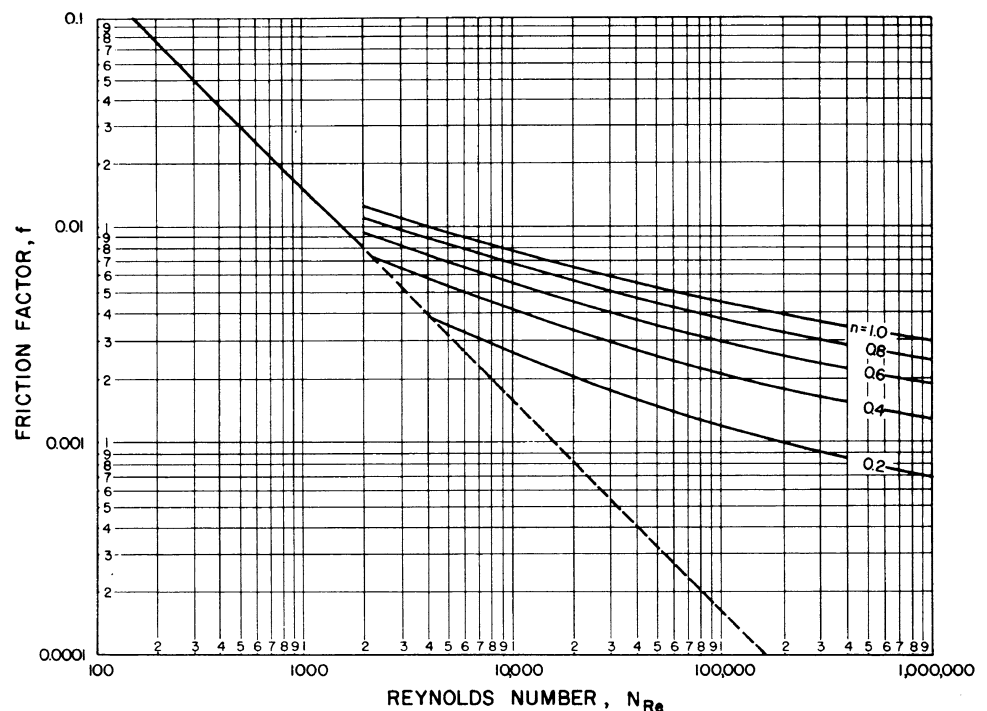
The pressure in front of the gas column can be expressed in terms of casing pressure, frictional pressure drop, and pressure change due to potential energy change, which is

$$p_2 = p_{\text{casing}} + \rho_m g L_{\text{wellhead-gas top}} - p_f \quad (15)$$

where p_{casing} = casing pressure, $L_{\text{wellhead-gas top}}$ = distance between wellhead and top of gas column.

Casing pressure is readily available during circulation. The calculation of frictional pressure drop is akin to the frictional pressure drop between bottomhole and base of gas column. In case of laminar flow, the frictional pressure drop is

Fig. 2 Friction factor for power-law fluid model, after Bourgoyne et al. (1986)



$$p_f = \frac{dp_f}{dh} L_{\text{wellhead-gas top}} = \frac{Ku_m^n \left(\frac{2+1/n}{0.0208}\right)^n}{144000(D_2 - D_1)^{1+n}} L_{\text{wellhead-gas top}} \quad (16)$$

If the flow is turbulent flow, the frictional pressure drop can be calculated by

$$p_f = \frac{dp_f}{dh} L_{\text{wellhead-gas top}} = \frac{f \rho_m u_m^2}{21.1(D_2 - D_1)} L_{\text{wellhead-gas top}} \quad (17)$$

Again, Reynolds number is calculated from Eq. (9) and friction factor is read from Fig. 2.

The drag force on the flank of the gas column can be derived according to the flow regime: laminar and turbulent flow conditions. When gas column moves upward along the annulus, the drag force on the flank of the gas column is

$$F_{D1} = A_{\text{gas column flank}} \tau_{\text{gm}} = \pi(D_1 + D_2) L_{\text{gas cylinder}} \tau_{\text{gm}} \quad (18)$$

where $A_{\text{gas column flank}}$ = surface area of flank of gas column, τ_{gm} = shear stress between gas and mud.

Shear stress between gas and mud is calculated through (Taitel 1995)

$$\tau_{\text{gm}} = \frac{f_i \rho_g u_g^2}{2} \quad (19)$$

where f_i = gas–mud interfacial friction factor, u_g = gas velocity, ρ_g = gas density.

Gas–mud interfacial friction factor is calculated by

$$f_i = C N_{\text{Re}}^{-n} \quad (20)$$

where $C = 16$ and $n = 1.0$ for laminar flow, and $C = 0.046$ and $n = 0.2$ for turbulent flow. If f_i from Eq. (20) is larger than 0.014, $f_i = 0.014$ should be used.

Reynolds number is calculated by

$$N_{\text{Re}} = \frac{\rho_g u_g (D_2 - D_1)}{\mu_g} \quad (21)$$

where μ_g = gas viscosity.

The drag force on the cone surface, F_{D2} , can be estimated by Ling's (2010) method. In Fig. 1, the cone of gas column experiences a drag force resulting from the viscous mud flow around the cone surface. The magnitude of drag force depends on the flow regime, laminar, or turbulent flow. For laminar flow, the drag force is calculated from Stokes law. Stokes law has shown that for creeping flow (Castleman 1926), the drag force is related to the gas cone velocity through the fluid by:

$$F_{D2} = 3\pi \left(\frac{D_2 - D_1}{2} \right) \frac{\pi \left(\frac{D_2 - D_1}{4} \right) 2\pi \left(\frac{D_1}{2} + \frac{D_2 - D_1}{4} \right)}{4\pi \left(\frac{D_2 - D_1}{4} \right)^2} \mu_g u_g = \frac{3}{4} \pi^2 (D_2 + D_1) \mu_g u_g. \quad (22)$$

Decomposing the drag force on the cone surface, we obtain vertical direction force, which is

$$F_{D2-\text{vert}} = \int_0^{90^\circ} F_{D2} \cos \theta d\theta = F_{D2} [\sin(90^\circ) - \sin(0^\circ)] = F_{D2} = \frac{3}{4} \pi^2 (D_2 + D_1) \mu_g u_g. \quad (23)$$

Equation (23) is found to give acceptable accuracy for Reynolds numbers below 0.1. For Reynolds numbers greater than 0.1, the drag force needs to be estimated using friction factor. The friction factor is defined by:

$$f = \frac{F_{D2}}{A_{\text{cone surface}} E_k} \quad (24)$$

where $A_{\text{cone surface}}$ = characteristic area of the cone of gas column, E_k = kinetic energy per unit volume.

Then, the drag force can be expressed as:

$$F_{D2} = f A_{\text{cone surface}} E_k \quad (25)$$

The characteristic area of the cone of gas column is given by:

$$A_{\text{cone surface}} = \frac{1}{4} \pi \left(\frac{D_2 - D_1}{4} \right) 2\pi \left(\frac{D_2 + D_1}{4} \right) = \frac{\pi^2}{32} (D_2^2 - D_1^2) \quad (26)$$

The kinetic energy per unit volume is given by:

$$E_k = \frac{\rho_g u_g^2}{2} \quad (27)$$

The friction factor f can be calculated by Eq. (20). If f_i from Eq. (20) is larger than 0.014, $f_i = 0.014$ should be used.

The gravity force resulting from the gas column is expressed as

$$F_G = \rho_{g,\text{BH}} g V_{\text{gas kick,BH}} \quad (28)$$

where

$$\rho_{g,\text{BH}} = \frac{p_p M}{z R T_{\text{BH}}} \quad (29)$$

M = molecular weight of gas, R = universal gas constant, z = gas deviation factor, T_{BH} = bottomhole temperature, $\rho_{g,\text{BH}}$ = gas density at bottomhole.

The molecular weight can be calculated from gas-specific gravity. Gas-specific gravity can be calculated from shut-in drillpipe pressure, shut-in casing pressure, mud density, and pit gain, or from offset well gas

property. Bottomhole temperature and temperature at any depth can be estimated using regional temperature gradient. Gravity force of gas column is constant during the gas migration.

Substituting Eqs. (6), (14), (18), (23), and (28) into (5), we have

$$\begin{aligned}
 F_{\text{net}} = & \pi \frac{D_2^2 - D_1^2}{4} p_1 - \pi \frac{D_2^2 - D_1^2}{4} p_2 \\
 & - \pi(D_1 + D_2)L_{\text{gas cylinder}} \tau_{\text{gm}} - \frac{3}{4} \pi^2 (D_2 + D_1) \mu_g u_g \\
 & - \rho_{g,\text{BH}} g V_{\text{gas kick,BH}} = \pi \left(\frac{D_2^2 - D_1^2}{4} \right) (p_1 - p_2) \\
 & - \pi(D_2 + D_1) u_g \left[L_{\text{gas cylinder}} \frac{8}{N_{\text{Re}}} \rho_g u_g + \frac{3}{4} \pi \mu_g \right] \\
 & - \rho_{g,\text{BH}} g V_{\text{gas kick,BH}}
 \end{aligned} \quad (30)$$

for laminar flow.

Substituting Eqs. (6), (14), (18), (25), and (28) into (5), we have

$$\begin{aligned}
 F_{\text{net}} = & \pi \frac{D_2^2 - D_1^2}{4} p_1 - \pi \frac{D_2^2 - D_1^2}{4} p_2 \\
 & - \pi(D_1 + D_2)L_{\text{gas cylinder}} \tau_{\text{gm}} - f A_{\text{cone surface}} E_k \\
 & - \rho_{g,\text{BH}} g V_{\text{gas kick,BH}} \\
 = & \pi \left(\frac{D_2^2 - D_1^2}{4} \right) (p_1 - p_2) - \pi(D_2 + D_1)L_{\text{gas cylinder}} \frac{0.046}{N_{\text{Re}}^{0.2}} \rho_g u_g^2 \\
 & - f \frac{\pi^2}{32} (D_2^2 - D_1^2) \frac{\rho_m u_g^2}{2} - \rho_{g,\text{BH}} g V_{\text{gas kick,BH}}
 \end{aligned} \quad (31)$$

for turbulent flow.

With the calculated net force, the acceleration of gas column can be calculated through

$$a = \frac{F_{\text{net}}}{m_g} = \frac{F_{\text{net}}}{\rho_{g,\text{BH}} V_{\text{gas kick,BH}}} \quad (32)$$

where a = acceleration, m_g = mass of gas column.

Therefore, substituting Eqs. (30) and (31) into (32) gives the governing equations for accelerations of gas column under laminar and turbulent flows, respectively.

$$a = \frac{\pi \left(\frac{D_2^2 - D_1^2}{4} \right) (p_1 - p_2) - \pi(D_2 + D_1) u_g \left[L_{\text{gas cylinder}} \frac{8}{N_{\text{Re}}} \rho_g u_g + \frac{3}{4} \pi \mu_g \right]}{\rho_{g,\text{BH}} V_{\text{gas kick,BH}}} - g \quad (33)$$

and

$$a = \frac{\pi \left(\frac{D_2^2 - D_1^2}{4} \right) (p_1 - p_2) - \pi(D_2 + D_1)L_{\text{gas cylinder}} \frac{0.046}{N_{\text{Re}}^{0.2}} \rho_g u_g^2 - f \frac{\pi^2}{32} (D_2^2 - D_1^2) \frac{\rho_m u_g^2}{2}}{\rho_{g,\text{BH}} V_{\text{gas kick,BH}}} - g \quad (34)$$

Calculation procedure

The calculation of gas column migrating up the annuli can be broken into the following steps:

- 1) Calculate the acceleration of gas column when it starts to migrate; at this moment, there is no drag force, so Eqs. (33) and (34) reduce to

$$a = \frac{\pi \left(\frac{D_2^2 - D_1^2}{4} \right) (p_1 - p_2)}{\rho_{g,\text{BH}} V_{\text{gas kick,BH}}} - g \quad (35)$$

- 2) Select a small 1st time step, Δt_1 , and calculate the velocity of gas column at the end of 1st time step by

$$u_g = a \Delta t_1 \quad (36)$$

- 3) Calculate the migrated distance, L_{migrated} , by

$$L_{\text{migrated}} = \frac{1}{2} a \Delta t_1^2 \quad (37)$$

- 4) Calculate the location of base of gas column, $h_{\text{gas base}}$, by

$$h_{\text{gas base}} = h_{\text{well}} - L_{\text{migrated}} \quad (38)$$

Table 1 Input data for gas kick migration calculation

Molecular weight of gas	20	lb/lb-mole
Gas specific gravity	0.69	air = 1.0
Well depth at kick occur	9,975	ft
Wellbore diameter	8.5	in.
Drillpipe length	9,445	ft
Drillpipe diameter (OD)	4.5	in.
Drill collar length	530	ft
Drill collar diameter (OD)	6.25	in.
Shut-in drillpipe pressure	275	psi
Shut-in casing pressure	448	psi
Bottomhole temperature	180	°F
Temperature gradient	1.1	°F/100 ft
Pit gains or kick volume at bottomhole	13.6	bbbl
Mud density	11.7	lbm/gal
The 300-rpm dial reading in mud viscometer	29	lb/100 ft ²
The 600-rpm dial reading in mud viscometer	46	lb/100 ft ²
Consistency index of mud	234	cp
Flow-behavior index of mud	0.67	
Mud pressure gradient	0.608	psi/ft
Mass of kick	1,304	lbm
Gravitational acceleration	31.174	ft/s ²
Bottomhole pressure	6,338	psi
Kick density at bottomhole	17.08	lbm/ft ³

- 5) Assuming a new gas volume, which is larger than gas volume at bottomhole; calculate the height of gas column, $h_{\text{gas kick}}$ through Eq. (3)
- 6) Calculate the location of center of gas column $h_{\text{gas center}}$, by

$$h_{\text{gas center}} = h_{\text{gas base}} - \frac{L_{\text{gas kick}}}{2} \quad (39)$$

- 7) Calculate the average pressure of gas column, \bar{p}_{gas}
- 8) Using real gas law, calculate the volume of gas kick at new location, which is

$$V_{\text{gas kick}} = \frac{z_{\text{BH}} T_{\text{BH}} \bar{p}_{\text{gas}}}{z T_p V_{\text{gas kick, BH}}} \quad (40)$$

where T = temperature at location, z_{BH} = gas deviation factor at bottomhole, Δt_l = 1st time step, L_{migrated} = gas migrated distance, $h_{\text{gas base}}$ = location of base of gas column, $h_{\text{gas center}}$ = location of center of gas column, \bar{p}_{gas} = average pressure of gas column.

- 9) If calculated gas volume is different from assumed volume in Step 5, repeat Steps 5 through 8 until a converged volume is obtained
- 10) With the gas column location after 1st time step, we can calculate the acceleration of gas column using Eq. (33) or (34)
- 11) Select 2nd time step and calculate the velocity and migrated distance at the end of 2nd time step
- 12) Repeat Steps 4 through 11 until base of gas column migrates to the surface

Case study to illustrate the validation and application of model

Field data from a gas kick detection and control in a well in Southeast Asia were used to verify the model. A kick was detected when the well was drilled to a depth of 9,975 ft. The well was shut in; the influx was contained and further entry of formation fluid was prevented. The pit gains were 13.6 bbl when the well was shut in. Shut-in casing and drillpipe pressures were recorded. The driller's method was used to circulate the kick out the hole and control the well. Table 1 shows the key parameters used in the calculations.

The calculated time for gas migrating to wellhead is 123.1 min. Field observed that it takes 129.3 min for gas migration. The absolute error is −6.2 min and the relative error is −4.8 %. The errors can be results of irregular borehole, inaccurate temperature profile in wellbore,

inaccurate measurement of pit gains, variation of mud properties along the wellbore, inaccurate kick properties, and any deviation from the aforementioned assumptions. Therefore, the model gives reasonable results.

A computer program is coded to calculate the rising of gas kick. Thus, the calculation can be done within acceptable time period after the well is shut in. Then, the calculation can provide a forecast of gas kick location versus circulating time for circulating kick out of hole operation. The real-time data during well control can be compared with the predicted values. Any deviation from forecast could be an indication of downhole problem. The proposed method can be combined with engineers experience to predict the downhole situation, shut-in casing pressure, and mud rate as functions of position of gas kick. Therefore, the new model is a valuable tool in well control.

Conclusions

Following conclusions can be drawn from this study:

The governing equation to estimate the gas kick migration velocity in the annuli has been developed.

The procedure to calculate the migration of gas kick from bottomhole to surface has been proposed.

Differences between forecast values and real-time data in well control could be signs of downhole problems.

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